## SFS



HTP and WR Technical Handbook

Revision Date
V1.01
March 2024

Changes
Initial Release

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## HTP \& WR

## 1. Overview

SFS HTP and WR are high-strength, self-tapping structural fasteners designed for use in wood-to-wood and steel-to-wood applications in heavy-timber (HTP), mass-timber (MT), and conventional light-frame wood construction. HTP and WR fasteners are available in varying diameters and lengths, partial thread (PT) and full thread (FT) configurations, and varying head configurations (Figures 1.3.A and 1.3.B). Partial thread HTP fasteners are equipped with shank ribs (knurl) near the bottom of the unthreaded shank. The shank ribs reduce the drive-in resistance and ensure a tight fit between the two connecting members.

### 1.1 Reference documents

SFS HTP and WR fasteners have been evaluated by the International Code Council Evaluation Services (ICC ES) and the European Technical Assessment (ETA-12/0062, April 15, 2019) and conform to all applicable provisions of the International Building Code (IBC), International Residential Code (IRC), and the governing Eurocodes. The design method and presentation in this guide is to be used with the following editions of the standard CSAO86 Engineering Design in Wood and the National Building Code of Canada.

- Current section of National Building Code of Canada
- CSA 086-19 Engineering design in wood

See section 1.4 for more details.

## 1. Overview

### 1.2 Design overview

The factored lateral resistance, $N_{r}$, the factored withdrawal resistance $P_{r w}$ and the factored head pull-through resistance, $\mathrm{P}_{\mathrm{r} h}$, provided in this guide assume standard-term loading ( $K d=1.00$ ), dry service condition ( $K_{\text {sF }}=1.00$ ), untreated wood $\left(K_{T}=1.00\right)$, and for wood members other than CLT
( $\mathrm{J}_{\mathrm{x}}=1.0$ ). For other conditions, these factored values should be adjusted accordingly by all applicable modification factors outlined in CSA 086 and described below:

```
Kd = load duration factor (CSA 086 Clause 12.2.1.7.1 & Clause 5.3.2)
    = 1.15 (short-term load duration)
    = 1.00 (standard term load duration)
    = 0.65 (long-term load duration)
K
    = 1.00 (moisture content of wood is dry (less than 19%) at time of fabrication and in-service)
    = N/A (not allowed/applicable for service conditions other than dry conditions)
K
    = 1.0 (for connections that are untreated)
    = N/A (not allowed/applicable for treated wood)
Jx = connection resistance factor (CSA 086 Clause 12.6.5.1.2 & Clause 12.6.6.1)
    = 1.0 (for all wood members other than CLT)
    = 0.9 (for CLT)
JE = end grain factor (CSA 086 Clause 12.6.6.1) (applicable for withdrawal only)
    = 1.00 (for all other cases)
    = 0.67 (in panel edge of CLT)
    = 0.75 (in end grain)
```

Table 1.3: Wood species vs relative density cross-reference

|  | Usage |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Wood species | Mean oven-dry relative density | Visually stressgraded lumber | Glue-laminated timber | "MSR or MEL E Grades of S-P-F" | CLT |
| Southern Pine | 0.55 | x | x | x | x |
| D Fir-Larch, Hem-Fir | 0.49 |  | $\times$ |  | x |
| D Fir-Larch | 0.47 |  |  | x |  |
| Spruce-Pine | 0.44 |  | $\times$ |  |  |
| Spruce-Pine-Fir | 0.42 |  |  | x | x |
| Northern Species | 0.35 |  |  |  | x |

## 1. Overview

### 1.4 Commentary on presented values:

### 1.4.1

The following characteristic values for physical properties presented in Table 2.1 and referenced elsewhere herein were derived from characteristic values established from European Technical Assessments (ETAs):

- Torsion
- Tensile, fu
- Yield, fy


### 1.4.2

The following factored resistance values represented herein were derived from characteristic values established in ETAs:

- Factored head pull-through resistance, $\mathrm{P}_{\mathrm{r}}$
- Factored withdrawal resistance, Prw


### 1.4.2.1

First, the characteristic values were converted to equivalent specified strengths (standard term adjustment) to be used in conjunction with CSA O86 as follows:

Specified strength $=$ characteristic value $\times 0.8 \quad($ Eq. $1-1)$

### 1.4.2.2

In accordance with Eurocode 5 (EC5), characteristic values are converted to design values via the equation:
characteristic value $\times \mathrm{K}_{\bmod } / \gamma_{m} \quad$ (Eq. 1-2)
where:
$\mathrm{K}_{\text {mod }}=$ modification factor for duration of load and moisture content per EC5, and
$\gamma_{\mathrm{m}}=$ material factor
An adjustment value was derived for the specified strengths to be used in conjunction with CSA 086 in wood connections, as follows:

```
\(\phi_{\text {equiv }}=1 / \gamma_{m} \quad\) (Eq. 1-3)
    \(=1 / 1.3\)
    \(=0.77\)
```

This was established as an equivalence value for the factored values represented herein.
Factored values presented herein are represented in standard term load duration ( $K d=1.0$ ), which can be adjusted to other load durations. The values presented in the tables may be used in conjunction with CSA 086 using the following basic calculation:

Other load durations $=$ factored value $\times$ Kd $\quad($ Eq. 1-4)

$$
=\text { factored value } \times 1.15 \text { for wind and seismic, for example }
$$

### 1.4.3

Factored tensile resistance, $T_{r}$, presented in physical property tables 2.8-2.10 represent the factored tensile strength of the steel fastener. Factored tensile strength is represented as follows herein are derived directly from the ETA with a $\phi$ of 0.8 as per CSA S16 for steel.

### 1.4.4

Factored lateral resistance calculated in accordance with CSA 086, section 12.6

Connection geometry requirements presented per ICC AC233

## 1. Overview

### 1.5 Geometry and material properties

The geometry of SFS HTP and WR fasteners is shown in Figures 1.5.A and 1.5.B and Table 1.5.A. The material properties are provided in Table 1.5.B.

Figure 1.5.A: HTP thread design and head styles


Figure 1.5.B: WR thread design and head styles


## HTP \& WR

## 1. Overview

Table 1.5.A: HTP and WR dimensions


[^0]
## 1. Overview

1.6 Product code


## Material

T = Tempered carbon steel
Product family
WR = Wood reinforcement: special large diameter, full thread
HTP = Heavy timber: core products for variety of timber connections

### 1.7 Connection matrix



## 1. Overview

### 1.8 Fastener matrix



## mannararnaro 300 mm

| 250 mm | 275 mm | 300 mm | 325 mm | 350 mm | 375 mm | 400 mm | 425 mm | 450 mm | 475 mm | 975 mm |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## 1. Overview

### 1.8 Fastener matrix continued

## HTP-T-CS-FT-8xL <br> 8 mm countersunk full thread <br> HTP-T-CS-FT-10xL <br> 10 mm countersunk full thread

Bramavinumunur 60 mm


HTP-T-CH-FT-6xL
6 mm cylinder head full thread

Benamanamanamanamanamanamanare 120 mm





$\square$ amanamanamanamamanamanaman 120 mm



| HTP-T-CH-CC-6xL |
| :--- |
| 6 mm cylinder head double thread 7 - |


HTP-T-CH-CC-8xL



|  | 0 mm | 25 mm | 50 mm | 75 mm | 100 mm | 125 mm | 150 mm | 175 mm | 200 mm | 225 mm |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| 250 mm | 275 mm | 300 mm | 325 mm | 350 mm | 375 mm | 400 mm | 425 mm | 450 mm | 475 mm | 975 mm | 1000 mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## 2. Reference design values

Table 2.1: HTP and WR material properties

| Screw | $\mathbf{d}(\mathbf{m m})$ | Torsion (Nm) | Tensile, $\mathbf{f}_{\mathbf{u}}(\mathbf{M P a})$ | ${\text { Yield, } \mathbf{f}_{\mathbf{y}}(\mathbf{M P a})}^{\mathbf{f}_{\mathbf{y}}{ }^{\mathbf{1}}(\mathbf{M P a})}$ |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| HTP 6 mm, partial thread | 6.0 | 11 | 1018 | 1073 | 1045 |
| HTP 6 mm , full thread |  |  |  | 802 | 910 |
| HTP 8 mm , partial and full thread | 8.0 | 25 | 920 | 826 | 873 |
| HTP 10 mm , partial and full thread | 10.0 | 42 | 978 | 885 | 932 |
| WR 13 mm , full thread | 13.0 | 100 | 967 | 779 | 873 |

${ }^{1}$ Average of $f_{u}$ and $f_{y}$ per CSA O86:19, 12.4.4.3.3.3. This is the rule used to calculate tables 2.2-2.7.

The reference lateral design values for SFS HTP and WR are provided in Tables 2.2-2.7. The factored withdrawal and factored head pull-through values are provided in Tables 2.8, 2.9 and 2.10 respectively. The appropriate modification factors shall be used as described in Section 1.2 of this design guide.

Figure 2.1


Table 2.2: Reference lateral design values-single shear wood-to-wood connection, partial thread

| Fastener Designation Diameter $\times$ Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member Dowel Bearing Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Partial Thread Screws in Wood-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.35 |  |  |  | 0.42 |  |  |  | 0.44 |  |  |  |
|  |  |  | Nr,\\| | Nr,\||/ | Nrı ${ }_{\text {ıU\\| }}$ | Nr, | Nr,\\|| | Nr, \||/ | $\mathrm{Nr}_{ \pm \perp \\|}$ | Nr, | Nr,\|| | Nr, ${ }_{\\| / 1}$ | Nr, $\mathrm{r}_{ \pm\\| \\|}$ | $\mathrm{Nr}_{\text {, }}$ |
| $6.0 \times 60$ | 13 | 38 | 0.444 | 0.246 | 0.258 | 0.195 | 0.532 | 0.296 | 0.309 | 0.234 | 0.558 | 0.310 | 0.324 | 0.245 |
| $6.0 \times 70$ | 19 | 41 | 0.532 | 0.369 | 0.328 | 0.234 | 0.638 | 0.443 | 0.394 | 0.281 | 0.668 | 0.464 | 0.412 | 0.294 |
| $6.0 \times 80$ |  | 51 | 0.609 |  | 0.367 | 0.273 | 0.685 |  | 0.440 | 0.327 | 0.706 |  | 0.461 | 0.343 |
| $6.0 \times 90$ | 25 | 55 | 0.665 | 0.444 | 0.437 | 0.312 | 0.752 | 0.496 | 0.524 | 0.374 | 0.776 | 0.511 | 0.549 | 0.392 |
| $6.0 \times 100$ |  | 65 |  |  | 0.476 | 0.350 |  |  | 0.571 | 0.420 |  |  | 0.598 | 0.440 |
| $6.0 \times 110$ |  | 75 |  |  | 0.514 | 0.389 |  |  | 0.617 | 0.439 |  |  | 0.647 | 0.452 |
| $6.0 \times 120$ | 38 | 72 | 0.777 | 0.493 | 0.616 | 0.428 | 0.887 | 0.555 | 0.739 | 0.498 | 0.917 | 0.573 | 0.774 | 0.514 |
| $6.0 \times 140$ | 51 | 80 | 0.883 | 0.542 | 0.690 | 0.490 | 0.967 | 0.614 | 0.756 | 0.557 | 0.990 | 0.635 |  | 0.576 |
| $6.0 \times 150$ | 64 | 77 |  | 0.591 |  | 0.539 |  | 0.674 |  | 0.616 |  | 0.696 |  | 0.638 |
| $6.0 \times 160$ | 76 | 74 |  | 0.633 |  | 0.580 |  | 0.723 |  | 0.641 |  | 0.748 |  | 0.657 |
| $6.0 \times 180$ | 89 | 81 |  | 0.661 |  | 0.586 |  | 0.756 |  |  |  | 0.774 |  |  |
| $6.0 \times 200$ | 114 | 76 |  | 0.640 |  |  |  | 0.732 |  |  |  | 0.758 |  |  |
| $6.0 \times 220$ | 140 | 71 |  | 0.619 |  | 0.567 |  | 0.707 |  |  |  | 0.731 |  |  |
| $6.0 \times 240$ | 152 | 78 |  | 0.647 |  | 0.586 |  | 0.741 |  |  |  | 0.767 |  |  |
| $6.0 \times 260$ | 178 | 73 |  | 0.626 |  | 0.574 |  | 0.715 |  |  |  | 0.740 |  |  |
| $6.0 \times 280$ | 191 | 80 |  | 0.655 |  | 0.586 |  | 0.749 |  |  |  | 0.774 |  |  |
| $6.0 \times 300$ | 216 | 74 |  | 0.634 |  | 0.581 |  | 0.724 |  |  |  | 0.750 |  |  |
| $8.0 \times 90$ | 19 | 58 | 0.878 | 0.480 | 0.508 | 0.386 | 1.025 | 0.576 | 0.610 | 0.463 | 1.055 | 0.604 | 0.639 | 0.485 |
| $8.0 \times 100$ | 25 | 61 | 0.988 | 0.640 | 0.599 | 0.437 | 1.112 | 0.750 | 0.719 | 0.524 | 1.147 | 0.772 | 0.754 | 0.549 |
| $8.0 \times 120$ | 38 | 69 | 1.133 | 0.737 | 0.782 | 0.537 | 1.287 | 0.827 | 0.938 | 0.645 | 1.330 | 0.852 | 0.983 | 0.676 |
| $8.0 \times 140$ | 51 | 76 | 1.279 | 0.801 | 0.964 | 0.638 | 1.461 | 0.904 | 1.157 | 0.766 | 1.513 | 0.932 | 1.212 | 0.802 |

## 2. Reference design values

Table 2.2: Continued

| Fastener <br> Designation <br> Diameter $\times$ <br> Length <br> (mm) | Side <br> Member Thickness, $t_{1}(\mathrm{~mm})$ | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Partial Thread Screws in Wood-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.35 |  |  |  | 0.42 |  |  |  | 0.44 |
|  |  |  | Nr, ${ }_{\text {,\| }}$ | Nr, ${ }_{\text {\|\|/ }}$ | $\mathrm{Nr}_{1\lrcorner \\|}$ | $\mathbf{N r}_{1}$ | $\mathrm{Nr}_{\text {,\|\| }}$ | Nr, \||/ | $\mathrm{Nr}_{1 \perp\\| \\|}$ | Nr, | Nr,\\|| | Nr, ${ }_{\text {\|\|/ }}$ | $\mathrm{Nr}_{1 \perp \\| \mid}$ | $\mathrm{Nr}_{\text {, }}$ |
| $8.0 \times 160$ | 51 | 96 | 1.279 | 0.801 | 1.065 | 0.718 | 1.461 | 0.904 | 1.193 | 0.813 | 1.513 | 0.932 | 1.221 | 0.840 |
| $8.0 \times 180$ | 64 | 103 | 1.393 | 0.865 | 1.089 | 0.782 | 1.526 | 0.981 |  | 0.890 | 1.562 | 1.013 |  | 0.920 |
| $8.0 \times 200$ | 89 | 98 |  | 0.993 |  | 0.910 |  | 1.134 |  | 1.012 |  | 1.174 |  | 1.036 |
| $8.0 \times 220$ | 102 | 105 |  | 1.057 |  | 0.924 |  | 1.193 |  |  |  |  |  |  |
| $8.0 \times 240$ | 127 | 100 |  | 1.047 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 260$ | 152 | 94 |  | 1.019 |  |  |  |  |  |  |  | 1.208 |  |  |
| $8.0 \times 280$ | 165 | 102 |  | 1.056 |  |  |  |  |  |  |  | 1.221 |  |  |
| $8.0 \times 300$ | 191 | 96 |  | 1.029 |  |  |  |  |  |  |  | 1.220 |  |  |
| $8.0 \times 320$ | 203 | 103 |  | 1.066 |  |  |  |  |  |  |  | 1.221 |  |  |
| $8.0 \times 340$ | 229 | 98 |  | 1.039 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 360$ | 241 | 105 |  | 1.075 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 380$ | 267 | 100 |  | 1.048 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 400$ | 292 | 95 |  | 1.021 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 420$ | 305 | 102 |  | 1.058 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 460$ | 343 | 104 |  | 1.067 |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 500$ | 381 | 106 |  | 1.077 |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 120$ | 25 | 79 | 1.423 | 0.773 | 0.829 | 0.633 | 1.596 | 0.928 | 0.995 | 0.759 | 1.643 | 0.972 | 1.043 | 0.795 |
| $10.0 \times 140$ | 38 | 86 | 1.599 | 1.070 | 1.049 | 0.754 | 1.807 | 1.196 | 1.259 | 0.905 | 1.864 | 1.231 | 1.319 | 0.948 |
| $10.0 \times 160$ | 51 | 93 | 1.775 | 1.147 | 1.270 | 0.876 | 2.017 | 1.289 | 1.523 | 1.051 | 2.085 | 1.328 | 1.596 | 1.101 |
| $10.0 \times 180$ | 64 | 100 | 1.950 | 1.224 | 1.490 | 0.998 | 2.228 | 1.382 | 1.788 | 1.197 | 2.306 | 1.425 | 1.873 | 1.254 |
| $10.0 \times 200$ | 89 | 95 | 2.144 | 1.379 | 1.676 | 1.119 | 2.348 | 1.567 | 1.836 | 1.343 | 2.403 | 1.620 | 1.879 | 1.407 |
| $\underline{10.0 \times 220}$ | 102 | 102 |  | 1.456 |  | 1.241 |  | 1.660 |  | 1.489 |  | 1.717 |  | 1.560 |
| $10.0 \times 240$ | 127 | 97 |  | 1.428 |  | 1.301 |  | 1.626 |  | 1.487 |  | 1.681 |  | 1.539 |
| $10.0 \times 260$ | 152 | 92 |  | 1.395 |  | 1.268 |  | 1.586 |  | 1.447 |  | 1.640 |  | 1.497 |
| $10.0 \times 280$ | 165 | 99 |  | 1.439 |  | 1.312 |  | 1.640 |  | 1.501 |  | 1.696 |  | 1.553 |
| $10.0 \times 300$ | 191 | 93 |  | 1.406 |  | 1.280 |  | 1.600 |  | 1.461 |  | 1.654 |  | 1.512 |
| $10.0 \times 320$ | 203 | 101 |  | 1.451 |  | 1.324 |  | 1.654 |  | 1.514 |  | 1.710 |  | 1.568 |
| $10.0 \times 340$ | 229 | 95 |  | 1.418 |  | 1.291 |  | 1.614 |  | 1.475 |  | 1.669 |  | 1.527 |
| $10.0 \times 360$ | 241 | 103 |  | 1.462 |  | 1.336 |  | 1.667 |  | 1.528 |  | 1.725 |  | 1.582 |
| $10.0 \times 380$ | 267 | 97 |  | 1.430 |  | 1.303 |  | 1.628 |  | 1.489 |  | 1.683 |  | 1.541 |
| $10.0 \times 400$ | 292 | 92 |  | 1.397 |  | 1.270 |  | 1.588 |  | 1.449 |  | 1.642 |  | 1.500 |
| $10.0 \times 420$ | 305 | 99 |  | 1.441 |  | 1.314 |  | 1.642 |  | 1.503 |  | 1.698 |  | 1.556 |
| $10.0 \times 460$ | 343 | 101 |  | 1.453 |  | 1.326 |  | 1.656 |  | 1.517 |  | 1.712 |  | 1.570 |
| $\underline{10.0 \times 480}$ | 381 | 83 |  | 1.343 |  | 1.216 |  | 1.523 |  | 1.384 |  | 1.574 |  | 1.432 |

## Notes:

${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
${ }^{2}$ Tabulated reference lateral design values, $\mathrm{N}_{\mathrm{r}}$ apply to screws driven into the side grain of the main member, such that the screws are oriented perpendicular to the grain and loaded as follows:

- $\mathrm{N}_{\mathrm{r}, \|}$ both side and main member are loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r},|/| \perp}$ side member loaded perpendicular to the grain and main member loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r}, 1 /| |}$ side member loaded parallel to the grain and main member loaded perpendicular to the grain. $-N_{r, \perp}$ both side and main member are loaded perpendicular to the grain.
${ }^{3}$ Tabulated lateral design values are based on both wood members having the same specific gravity, G
${ }^{4}$ The value $f_{y}$ used in calculating tables 2.2-2.7 is the value $f_{y}{ }^{1}$ from Table 2.1
${ }^{5}$ Main member dowel bearing length, $t_{2}$ is defined as fastener penetration into the main member minus the length of the tapered tip of the screw.


## HTP \& WR

## 2. Reference design values

Table 2.2: Continued

| Fastener <br> Designation <br> Diameter $\times$ <br> Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member Dowel Bearing Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Partial Thread Screws in Wood-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.47 |  |  |  | 0.49 |  |  |  | 0.55 |
|  |  |  | Nr,\|| | Nr,\||1 | Nr, $1 / \\|$ | Nr, | Nr,\|| | Nr,\||| | $\mathrm{Nr}_{ \pm \perp \\|}$ | Nr, | Nr,\|| | Nr,\||/ | $\mathrm{Nr}_{ \pm\lrcorner \\|}$ | Nr, |
| $6.0 \times 60$ | 13 | 38 | 0.596 | 0.331 | 0.346 | 0.262 | 0.621 | 0.345 | 0.361 | 0.273 | 0.697 | 0.387 | 0.405 | 0.307 |
| $6.0 \times 70$ | 19 | 41 | 0.714 | 0.496 | 0.440 | 0.314 | 0.744 | 0.512 | 0.459 | 0.328 | 0.817 | 0.549 | 0.515 | 0.368 |
| $6.0 \times 80$ |  | 51 | 0.737 |  | 0.493 | 0.366 | 0.757 |  | 0.513 | 0.382 |  |  | 0.576 | 0.429 |
| $6.0 \times 90$ | 25 | 55 | 0.812 | 0.532 | 0.587 | 0.418 | 0.836 | 0.546 | 0.612 | 0.436 | 0.905 | 0.587 | 0.687 | 0.490 |
| $6.0 \times 100$ |  | 65 |  |  | 0.639 | 0.470 |  |  | 0.666 | 0.484 |  |  | 0.747 | 0.522 |
| $6.0 \times 110$ |  | 75 |  |  | 0.691 | 0.472 |  |  | 0.720 |  |  |  | 0.784 |  |
| $6.0 \times 120$ | 38 | 72 | 0.962 | 0.598 | 0.800 | 0.538 | 0.992 | 0.615 | 0.817 | 0.553 | 1.081 | 0.665 | 0.865 | 0.599 |
| $6.0 \times 140$ | 51 | 80 | 1.023 | 0.664 |  | 0.604 | 1.045 | 0.684 |  | 0.622 | 1.107 | 0.742 |  | 0.677 |
| $6.0 \times 150$ | 64 | 77 |  | 0.731 |  | 0.670 |  | 0.753 |  | 0.691 |  | 0.820 |  | 0.734 |
| $6.0 \times 160$ | 76 | 74 |  | 0.786 |  | 0.679 |  | 0.811 |  | 0.693 |  | 0.865 |  |  |
| $6.0 \times 180$ | 89 | 81 |  | 0.800 |  |  |  | 0.817 |  |  |  |  |  |  |
| $6.0 \times 200$ | 114 | 76 |  | 0.796 |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 220$ | 140 | 71 |  | 0.768 |  |  |  | 0.792 |  |  |  |  |  |  |
| $6.0 \times 240$ | 152 | 78 |  | 0.800 |  |  |  | 0.817 |  |  |  |  |  |  |
| $6.0 \times 260$ | 178 | 73 |  | 0.778 |  |  |  | 0.802 |  |  |  |  |  |  |
| $6.0 \times 280$ | 191 | 80 |  | 0.800 |  |  |  | 0.817 |  |  |  |  |  |  |
| $6.0 \times 300$ | 216 | 74 |  | 0.787 |  |  |  | 0.812 |  |  |  |  |  |  |
| $8.0 \times 90$ | 19 | 58 | 1.100 | 0.645 | 0.683 | 0.519 | 1.130 | 0.672 | 0.712 | 0.541 | 1.216 | 0.754 | 0.799 | 0.607 |
| $8.0 \times 100$ | 25 | 61 | 1.198 | 0.803 | 0.805 | 0.586 | 1.232 | 0.824 | 0.839 | 0.611 | 1.330 | 0.884 | 0.942 | 0.686 |
| $8.0 \times 120$ | 38 | 69 | 1.393 | 0.889 | 1.050 | 0.722 | 1.435 | 0.913 | 1.094 | 0.752 | 1.559 | 0.984 | 1.228 | 0.844 |
| $8.0 \times 140$ | 51 | 76 | 1.589 | 0.975 | 1.262 | 0.857 |  | 1.003 | 1.289 | 0.893 | 1.747 |  | 1.365 | 0.982 |
| $8.0 \times 160$ |  | 96 |  |  |  | 0.879 |  |  |  | 0.905 |  |  |  |  |
| $8.0 \times 180$ | 64 | 103 | 1.614 | 1.061 |  | 0.965 | 1.648 | 1.092 |  | 0.995 |  | 1.186 |  | 1.082 |
| $8.0 \times 200$ | 89 | 98 |  | 1.233 |  | 1.071 |  | 1.272 |  | 1.093 |  | 1.365 |  | 1.159 |
| $8.0 \times 220$ | 102 | 105 |  | 1.262 |  |  |  | 1.289 |  |  |  |  |  |  |
| $8.0 \times 240$ | 127 | 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 260$ | 152 | 94 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 280$ | 165 | 102 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 300$ | 191 | 96 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 320$ | 203 | 103 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 340$ | 229 | 98 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 360$ | 241 | 105 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 380$ | 267 | 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 400$ | 292 | 95 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 420$ | 305 | 102 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 460$ | 343 | 104 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 500$ | 381 | 106 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 120$ | 25 | 79 | 1.714 | 1.038 | 1.114 | 0.849 | 1.760 | 1.082 | 1.161 | 0.886 | 1.896 | 1.215 | 1.303 | 0.994 |
| $10.0 \times 140$ | 38 | 86 | 1.950 | 1.282 | 1.409 | 1.013 | 2.006 | 1.316 | 1.469 | 1.056 | 2.172 | 1.415 | 1.649 | 1.185 |
| $\underline{10.0 \times 160}$ | 51 | 93 | 2.186 | 1.386 | 1.705 | 1.176 | 2.252 | 1.424 | 1.777 | 1.226 | 2.448 | 1.536 | 1.995 | 1.377 |
| $10.0 \times 180$ | 64 | 100 | 2.422 | 1.490 | 1.942 | 1.340 | 2.498 | 1.532 | 1.983 | 1.382 | 2.687 | 1.658 | 2.101 | 1.499 |
| $10.0 \times 200$ | 89 | 95 | 2.484 | 1.698 |  | 1.503 | 2.536 | 1.749 |  | 1.567 |  | 1.901 |  | 1.742 |
| $10.0 \times 220$ | 102 | 102 |  | 1.801 |  | 1.648 |  | 1.857 |  | 1.682 |  | 2.022 |  | 1.782 |

## 2. Reference design values

Table 2.2: Continued

| Fastener <br> Designation <br> Diameter $\times$ <br> Length <br> (mm) | Side <br> Member Thickness, $t_{1}(\mathrm{~mm})$ | Main Member Dowel Bearing Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Partial Thread Screws in Wood-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.47 |  |  |  | 0.49 |  |  |  | 0.55 |
|  |  |  | $\mathrm{Nr}_{\text {, }}$ | Nr, ${ }_{\text {\|\|/ }}$ | $\mathrm{Nr}_{\text {, }}$ | Nr, | Nr, ${ }_{\text {\|\| }}$ | Nr, \||/ | $\mathrm{Nr}_{\text {, }}$ | Nr, | $\mathrm{Nr}_{\text {,\|\| }}$ | Nr,\||/ | $\mathrm{Nr}_{\text {, }}$ | Nr, |
| $10.0 \times 240$ | 127 | 97 | 2.484 | 1.763 | 1.942 | 1.616 | 2.536 | 1.817 | 1.983 | 1.667 | 2.687 | 1.977 | 2.101 | 1.782 |
| $10.0 \times 260$ | 152 | 92 |  | 1.719 |  | 1.572 |  | 1.771 |  | 1.621 |  | 1.926 |  | 1.767 |
| $10.0 \times 280$ | 165 | 99 |  | 1.779 |  | 1.632 |  | 1.833 |  | 1.682 |  | 1.996 |  | 1.782 |
| $10.0 \times 300$ | 191 | 93 |  | 1.735 |  | 1.587 |  | 1.787 |  | 1.637 |  | 1.944 |  |  |
| $10.0 \times 320$ | 203 | 101 |  | 1.794 |  | 1.647 |  | 1.850 |  | 1.682 |  | 2.014 |  |  |
| $10.0 \times 340$ | 229 | 95 |  | 1.750 |  | 1.603 |  | 1.804 |  | 1.653 |  | 1.962 |  |  |
| $10.0 \times 360$ | 241 | 103 |  | 1.810 |  | 1.648 |  | 1.866 |  | 1.682 |  | 2.032 |  |  |
| $10.0 \times 380$ | 267 | 97 |  | 1.766 |  | 1.619 |  | 1.820 |  | 1.670 |  | 1.980 |  |  |
| $10.0 \times 400$ | 292 | 92 |  | 1.721 |  | 1.574 |  | 1.774 |  | 1.624 |  | 1.929 |  | 1.769 |
| $10.0 \times 420$ | 305 | 99 |  | 1.781 |  | 1.634 |  | 1.836 |  | 1.682 |  | 1.998 |  | 1.782 |
| $10.0 \times 460$ | 343 | 101 |  | 1.797 |  | 1.648 |  | 1.852 |  |  |  | 2.017 |  |  |
| $10.0 \times 480$ | 381 | 83 |  | 1.649 |  | 1.502 |  | 1.698 |  | 1.548 |  | 1.843 |  | 1.684 |

Notes:
${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
${ }^{2}$ Tabulated reference lateral design values, $N_{r}$ apply to screws driven into the side grain of the main member, such that the screws are oriented perpendicular to the grain and loaded as follows:

- $\mathrm{N}_{\mathrm{r}, \|}$ both side and main member are loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r}, \mid / / \perp}$ side member loaded perpendicular to the grain and main member loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r}, 1 /| |}$ side member loaded parallel to the grain and main member loaded perpendicular to the grain.
- $\mathrm{N}_{\mathrm{r}, \perp}$ both side and main member are loaded perpendicular to the grain.
${ }^{3}$ Tabulated lateral design values are based on both wood members having the same specific gravity, G.
${ }^{4}$ The value $f_{y}$ used in calculating tables $2.2-2.7$ is the value $f_{y}{ }^{1}$ from Table 2.1
${ }^{5}$ Main member dowel bearing length, $t_{2}$ is defined as fastener penetration into the main member minus the length of the tapered tip of the screw.


## 2. Reference design values

The reference lateral design values for SFS HTP and WR are provided in Tables 2.22.7. The factored withdrawal and factored head pull-through values are provided in Tables 2.8, 2.9 and 2.10 respectively. The appropriate modification values shall be used as described in Section 1.2 of this design guide.

Figure 2.2


Table 2.3: Reference lateral design values-single shear wood-to-wood connection, full thread

| Fastener <br> Designation <br> Diameter $\times$ <br> Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full thread Screws in Wood-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.35 |  |  |  | 0.42 |  |  |  | 0.44 |  |  |  |
|  |  |  | Nr,\|| | Nr,\||/ | $\mathrm{Nr}_{1 \pm \\|}$ | Nr, | Nr,\|| | $\mathrm{Nr}_{\\|\| \| / \perp}$ | $\mathrm{Nr}_{1\lrcorner\\| \\|}$ | Nr, | $\mathrm{Nr}_{\text {, }}$ | $\mathrm{Nr}_{\\|\| \| / \perp}$ | $\mathrm{Nr}_{ \pm} \mathrm{III}$ | Nr, ${ }^{\text {d }}$ |
| $6.0 \times 60$ | 25 | 25 | 0.380 | 0.274 | 0.274 | 0.167 | 0.456 | 0.328 | 0.328 | 0.201 | 0.478 | 0.344 | 0.344 | 0.210 |
| $6.0 \times 80$ |  | 45 | 0.493 | 0.321 | 0.340 | 0.234 | 0.560 | 0.360 | 0.409 | 0.281 | 0.579 | 0.371 | 0.428 | 0.294 |
| $6.0 \times 100$ | 38 | 52 | 0.592 | 0.364 | 0.463 | 0.301 | 0.664 | 0.412 | 0.519 | 0.361 | 0.680 | 0.425 | 0.531 | 0.378 |
| $6.0 \times 120$ |  | 72 |  |  | 0.474 | 0.328 |  |  |  | 0.373 |  |  |  | 0.385 |
| $6.0 \times 140$ |  | 92 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 160$ | 50 | 100 | 0.606 | 0.404 |  |  |  | 0.460 |  | 0.421 |  | 0.476 |  | 0.436 |
| $8.0 \times 100$ | 38 | 49 | 0.910 | 0.626 | 0.623 | 0.401 | 1.093 | 0.704 | 0.748 | 0.481 | 1.145 | 0.725 | 0.784 | 0.504 |
| $8.0 \times 120$ | 50 | 57 | 1.100 | 0.681 | 0.786 | 0.493 | 1.259 | 0.770 | 0.943 | 0.591 | 1.293 | 0.795 | 0.988 | 0.619 |
| $8.0 \times 160$ | 60 | 87 | 1.153 | 0.727 | 0.901 | 0.659 | 1.263 | 0.825 | 0.987 | 0.750 |  | 0.853 | 1.011 | 0.776 |
| $8.0 \times 180$ |  | 107 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 200$ | 76 | 111 |  | 0.801 |  | 0.732 |  | 0.914 |  | 0.838 |  | 0.945 |  | 0.858 |
| $8.0 \times 220$ | 100 | 107 |  | 0.901 |  | 0.765 |  | 0.987 |  |  |  | 1.011 |  |  |
| $8.0 \times 240$ | 114 | 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 260$ | 120 | 127 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 280$ | 138 | 129 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 300$ |  | 149 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 340$ | 152 | 175 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 380$ | 175 | 192 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 120$ | 38 | 66 | 1.280 | 0.860 | 0.825 | 0.563 | 1.478 | 0.963 | 0.990 | 0.676 | 1.526 | 0.992 | 1.037 | 0.708 |
| $10.0 \times 160$ | 50 | 94 | 1.452 | 0.925 | 1.124 | 0.780 | 1.655 | 1.041 | 1.349 | 0.933 | 1.711 | 1.074 | 1.413 | 0.963 |
| $10.0 \times 200$ | 76 | 108 | 1.673 | 1.065 | 1.308 | 0.966 | 1.833 | 1.210 | 1.433 | 1.102 | 1.876 | 1.251 | 1.467 | 1.140 |
| $10.0 \times 220$ | 100 | 104 |  | 1.195 |  | 1.096 |  | 1.366 |  | 1.216 |  | 1.414 |  | 1.244 |
| $10.0 \times 240$ | 114 | 110 |  | 1.250 |  | 1.110 |  | 1.431 |  |  |  | 1.467 |  |  |
| $10.0 \times 260$ | 120 | 124 |  | 1.304 |  |  |  | 1.433 |  |  |  |  |  |  |
| $10.0 \times 280$ |  | 144 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 300$ | 138 | 146 |  | 1.308 |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 340$ | 152 | 172 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 380$ | 165 | 199 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 400$ | 190 | 193 | 2.966 | 2.319 | 2.319 | 1.967 | 3.249 | 2.540 | 2.540 | 2.155 | 3.325 | 2.600 | 2.600 | 2.206 |
| $13.0 \times 500$ | 215 | 268 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 600$ | 228 | 355 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 700$ | 240 | 443 |  |  |  |  |  |  |  |  |  |  |  |  |

## 2. Reference design values

Table 2.3 Continued

| Fastener <br> Designation <br> Diameter $\times$ <br> Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member <br> Dowel Bearing Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Wood-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.35 |  |  |  | 0.42 |  |  |  | 0.44 |  |  |  |
|  |  |  | Nr,\|| | Nr, ${ }_{\\| / 1}$ | $\mathrm{Nr}_{ \pm \perp \\|}$ | Nr, | Nr,\|| | Nr,\||/ | $\mathrm{Nr}_{1 \perp \\|}$ | Nr, | Nr,\|| | Nr,\||/ | $\mathrm{Nr}_{1\lrcorner \\|}$ | Nr, |
| $13.0 \times 800$ | 260 | 523 | 2.966 | 2.319 | 2.319 | 1.967 | 3.249 | 2.540 | 2.540 | 2.155 | 3.325 | 2.600 | 2.600 | 2.206 |
| $13.0 \times 900$ | 292 | 591 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 1000$ | 330 | 653 |  |  |  |  |  |  |  |  |  |  |  |  |

Notes:
${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
${ }^{2}$ Tabulated reference lateral design values, $N_{r}$ apply to screws driven into the side grain of the main member, such that the screws are oriented perpendicular to the grain and loaded as follows:

- $\mathrm{N}_{\mathrm{r}, \boldsymbol{\|}}$ both side and main member are loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r},| | / \perp}$ side member loaded perpendicular to the grain and main member loaded parallel to the grain.
$-\mathrm{N}_{\mathrm{r}, 1 /| |}$ side member loaded parallel to the grain and main member loaded perpendicular to the grain.
- $\mathrm{N}_{\mathrm{r}, \perp}$ both side and main member are loaded perpendicular to the grain.
${ }^{3}$ Tabulated lateral design values are based on both wood members having the same specific gravity, G.
${ }^{4}$ The value $\mathrm{f}_{\mathrm{y}}$ used in calculating tables 2.2-2.7 is the value $\mathrm{f}_{\mathrm{y}}{ }^{1}$ from Table 2.1
${ }^{5}$ Main member dowel bearing length, $t_{2}$ is defined as fastener penetration into the main member minus the length of the tapered tip of the screw.

Table 2.3 Continued

| Fastener <br> Designation <br> Diameter x <br> Length <br> (mm) | Side <br> Member <br> Thickness, $\mathrm{t}_{1}(\mathrm{~mm})$ | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ <br> (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Wood-Wood Connections for Specific Gravities of 1, 2,3,4 |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.47 |  |  |  | 0.49 |  |  |  | 0.55 |  |  |  |
|  |  |  | Nr, ${ }_{\text {, }}$ | $\mathbf{N r} \mathbf{r l \| l \| ~}$ | $\mathbf{N r} \mathrm{r}_{\perp / \\|}$ | Nr, | Nr, ${ }_{\text {\|l }}$ | Nr, $\mid / \perp$ | $\mathbf{N r}$, $\perp / \\|$ | Nr, | Nr, ${ }_{\text {, }}$ | Nr ${ }_{\\|/\\|}$ | $\mathbf{N r}, \pm \\|$ | Nr, |
| $6.0 \times 60$ | 25 | 25 | 0.510 | 0.367 | 0.367 | 0.224 | 0.532 | 0.383 | 0.383 | 0.234 | 0.597 | 0.428 | 0.430 | 0.263 |
| $6.0 \times 80$ |  | 45 | 0.606 | 0.387 | 0.457 | 0.314 | 0.625 | 0.397 | 0.477 | 0.328 | 0.679 |  | 0.535 | 0.368 |
| $6.0 \times 100$ | 38 | 52 | 0.703 | 0.445 | 0.549 | 0.404 | 0.717 | 0.458 | 0.561 | 0.416 | 0.760 | 0.497 | 0.594 | 0.452 |
| $6.0 \times 120$ |  | 72 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 140$ |  | 92 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 160$ | 50 | 100 |  | 0.499 |  | 0.458 |  | 0.514 |  | 0.472 |  | 0.560 |  | 0.504 |
| $8.0 \times 100$ | 38 | 49 | 1.202 | 0.757 | 0.837 | 0.538 | 1.239 | 0.778 | 0.873 | 0.561 | 1.348 | 0.840 | 0.979 | 0.630 |
| $8.0 \times 120$ | 50 | 57 | 1.336 | 0.831 | 1.045 | 0.662 | 1.364 | 0.856 | 1.067 | 0.690 | 1.445 | 0.927 | 1.130 | 0.774 |
| $8.0 \times 160$ | 60 | 87 |  | 0.893 |  | 0.814 |  | 0.920 |  | 0.839 |  | 0.999 |  | 0.914 |
| $8.0 \times 180$ |  | 107 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 200$ | 76 | 111 |  | 0.992 |  | 0.886 |  | 1.023 |  | 0.905 |  | 1.115 |  | 0.959 |
| $8.0 \times 220$ | 100 | 107 |  | 1.045 |  |  |  | 1.067 |  |  |  | 1.130 |  |  |
| $8.0 \times 240$ | 114 | 113 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 260$ | 120 | 127 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 280$ | 138 | 129 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 300$ |  | 149 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 340$ | 152 | 175 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 380$ | 175 | 192 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 120$ | 38 | 66 | 1.597 | 1.034 | 1.108 | 0.756 | 1.645 | 1.062 | 1.155 | 0.788 | 1.784 | 1.143 | 1.296 | 0.885 |
| $10.0 \times 160$ | 50 | 94 | 1.796 | 1.121 | 1.510 | 1.007 | 1.851 | 1.153 | 1.548 | 1.036 | 2.016 | 1.245 | 1.640 | 1.121 |
| $10.0 \times 200$ | 76 | 108 | 1.939 | 1.310 | 1.516 | 1.196 | 1.980 | 1.350 |  | 1.233 | 2.098 | 1.466 |  | 1.342 |
| $10.0 \times 220$ | 100 | 104 |  | 1.485 |  | 1.286 |  | 1.532 |  | 1.313 |  | 1.640 |  | 1.391 |
| $10.0 \times 240$ | 114 | 110 |  | 1.516 |  |  |  | 1.548 |  |  |  |  |  |  |
| $10.0 \times 260$ | 120 | 124 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 280$ |  | 144 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 300$ | 138 | 146 |  |  |  |  |  |  |  |  |  |  |  |  |

## 2. Reference design values

## Table 2.3 Continued

| Fastener Designation Diameter $\times$ Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Wood-Wood Connections for Specific Gravities of 1,2,3, |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.47 |  |  |  | 0.49 |  |  |  | 0.55 |
|  |  |  | $\mathrm{Nr}_{\text {, }}$ | $\mathrm{Nr}_{\text {,\|\| }}$ | $\mathrm{Nr}_{1 \perp \\|}$ | Nr, | Nr,\|| | Nr,\||/ | $\mathrm{Nr}_{ \pm \triangle \\|}$ | Nr, | Nr, ${ }_{\text {\|\| }}$ | $\mathrm{Nr}_{\text {,\|\| }}$ | $\mathrm{Nr}_{ \pm}$\\| | Nr, |
| $10.0 \times 340$ | 152 | 172 | 1.939 | 1.516 | 1.516 | 1.286 | 1.980 | 1.548 | 1.548 | 1.313 | 2.098 | 1.640 | 1.640 | 1.391 |
| $10.0 \times 380$ | 165 | 199 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 400$ | 190 | 193 | 3.437 | 2.687 | 2.687 | 2.280 | 3.509 | 2.743 | 2.743 | 2.328 | 3.718 | 2.906 | 2.906 | 2.466 |
| $13.0 \times 500$ | 215 | 268 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 600$ | 228 | 355 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 700$ | 240 | 443 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 800$ | 260 | 523 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 900$ | 292 | 591 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 1000$ | 330 | 653 |  |  |  |  |  |  |  |  |  |  |  |  |

Notes:
${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
 loaded as follows:

- $N_{r, \|}$ both side and main member are loaded parallel to the grain.
- $N_{r, \| / \perp}$ side member loaded perpendicular to the grain and main member loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r}, 1 / \|}$ side member loaded parallel to the grain and main member loaded perpendicular to the grain.
- $N_{r, \perp}$ both side and main member are loaded perpendicular to the grain.
${ }^{3}$ Tabulated lateral design values are based on both wood members having the same specific gravity, $G$.
${ }^{4}$ The value $f_{y}$ used in calculating tables $2.2-2.7$ is the value $f_{y}{ }^{1}$ from Table 2.1
${ }^{5}$ Main member dowel bearing length, $t_{2}$ is defined as fastener penetration into the main member minus the length of the tapered tip of the screw.


## 2. Reference design values

The reference lateral design values for SFS HTP and WR are provided in Tables 2.22.7. The factored withdrawal and factored head pull-through values are provided in Tables 2.8, 2.9 and 2.10 respectively. The appropriate modification values shall be used as described in Section 1.2 of this design guide.

Figure 2.3


Table 2.4: Reference lateral design values-single shear steel-to-wood connection, partial thread

| Fastener Designation | Side Member | Main Member Dowel |  |  | tored | ateral | Resista | ace (kN) | $\text { 1) for } \mathrm{Pa}$ Conne | rtial tions | ead | crews ific Gr | inte vitie | Nood <br> $1,2,3,4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter x |  | Bearing |  | 0.35 |  | 0.42 |  | 0.44 |  | 0.47 |  | 0.49 |  | 0.55 |
| (mm) |  | $\begin{aligned} & \mathrm{th}^{5}, \mathrm{t}_{\mathbf{2}} \\ & (\mathrm{mm}) \end{aligned}$ | Nr, ${ }_{\text {\|\| }}$ | Nr, | Nr, ${ }_{\text {\|l }}$ | Nr, | Nr, ${ }_{\text {\|\| }}$ | Nr, ${ }^{1}$ | Nr, ${ }_{\text {\|\| }}$ | Nr, | Nr, ${ }_{\text {\|\| }}$ | Nr, | Nr, ${ }_{\text {, }}$ | Nr, |
| $6.0 \times 60$ | 6 | 44 | 1.243 | 0.826 | 1.360 | 0.905 | 1.392 | 0.926 | 1.438 | 0.957 | 1.468 | 0.977 | 1.554 | 1.035 |
| $6.0 \times 70$ |  | 54 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 80$ |  | 64 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 90$ |  | 74 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 100$ |  | 84 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 110$ |  | 94 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 120$ |  | 104 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 140$ |  | 124 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 150$ |  | 134 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 160$ |  | 144 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 180$ |  | 164 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 200$ |  | 184 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 220$ |  | 204 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 240$ |  | 224 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 260$ |  | 244 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 280$ |  | 264 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 300$ |  | 284 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 80$ |  | 60 | 1.961 | 1.304 | 2.147 | 1.428 | 2.197 | 1.462 | 2.269 | 1.510 | 2.317 | 1.542 | 2.452 | 1.633 |
| $8.0 \times 90$ |  | 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 100$ |  | 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 120$ |  | 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 140$ |  | 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 160$ |  | 140 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 180$ |  | 160 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 200$ |  | 180 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 220$ |  | 200 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 240$ |  | 220 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 260$ |  | 240 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 280$ |  | 260 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 300$ |  | 280 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 320$ |  | 300 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 340$ |  | 320 |  |  |  |  |  |  |  |  |  |  |  |  |

## 2. Reference design values

Table 2.4: Continued

| Fastener <br> Designation <br> Diameter x <br> Length <br> (mm) | Side <br> Member <br> Thickness, $\mathrm{t}_{1}$ (mm) | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ <br> (mm) | Factored Lateral Resistance (kN) for Partial Thread Screws in Steel-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 0.35 |  | 0.42 |  | 0.44 |  | 0.47 |  | 0.49 |  | 0.55 |
|  |  |  | Nr, ${ }_{\text {,\| }}$ | Nr, | Nr, ${ }_{\text {, }}$ | Nr, | Nr,II | $\mathbf{N r} \mathbf{r l}$ | Nr, | Nr, | Nr, ${ }_{\text {II }}$ | $\mathbf{N r} \mathbf{r}_{\perp}$ | Nr, ${ }_{\text {II }}$ | Nr ${ }_{\text {, }}$ |
| $8 \times 360$ | 6 | 340 | 1.961 | 1.304 | 2.147 | 1.428 | 2.197 | 1.462 | 2.269 | 1.510 | 2.317 | 1.542 | 2.452 | 1.633 |
| $8 \times 380$ |  | 360 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8 \times 400$ |  | 380 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8 \times 420$ |  | 400 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8 \times 460$ |  | 440 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8 \times 500$ |  | 480 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 80$ |  | 58 | 3.018 | 1.765 | 3.303 | 2.118 | 3.380 | 2.219 | 3.492 | 2.324 | 3.564 | 2.373 | 3.773 | 2.513 |
| $10 \times 100$ |  | 78 |  | 2.007 |  | 2.198 |  | 2.249 |  |  |  |  |  |  |
| $10 \times 120$ |  | 98 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 140$ |  | 118 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 160$ |  | 138 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 180$ |  | 158 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 200$ |  | 178 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 220$ |  | 198 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 240$ |  | 218 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 260$ |  | 238 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 280$ |  | 258 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 300$ |  | 278 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 320$ |  | 298 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 340$ |  | 318 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 360$ |  | 338 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 380$ |  | 358 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 400$ |  | 378 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 420$ |  | 398 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 460$ |  | 438 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10 \times 480$ |  | 458 |  |  |  |  |  |  |  |  |  |  |  |  |

Notes:
${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
${ }^{2}$ Tabulated reference lateral design values, $\mathrm{N}_{\mathrm{r}}$ apply to screws driven into the side grain of the main member, such that the screws are oriented perpendicular to the grain and loaded as follows:

- $\mathrm{N}_{\mathrm{r}, \|}$ main member is loaded parallel to the grain.
- $N_{r, \perp}$ main member is loaded perpendicular to the grain.
${ }^{3}$ Tabulated lateral design values are based on side member dowel bearing strength of 450 MPa for ASTM A36 steel
${ }^{4}$ The value $f_{y}$ used in calculating tables $2.2-2.7$ is the value $f_{y}{ }^{1}$ from Table 2.1
${ }^{5}$ Main member dowel bearing length, $\mathrm{t}_{2}$ is defined as fastener penetration into the main member minus the length of the tapered tip of the screw.


## 2. Reference design values

The reference lateral design values for SFS HTP and WR are provided in Tables 2.22.7. The factored withdrawal and factored head pull-through values are provided in Tables 2.8, 2.9 and 2.10 respectively. The appropriate modification values shall be used as described in Section 1.2 of this design guide.

Figure 2.4


Table 2.5: Reference lateral design values-single shear steel-to-wood connection, full thread

| Fastener Designation Diameter $\times$ Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Steel-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 0.35 |  | 0.42 |  | 0.44 |  | 0.47 |  | 0.49 |  | 0.55 |
|  |  |  | Nr, \|| | Nr, | Nr, ${ }_{\text {,\|l }}$ | Nr, | Nr,\|| | Nr, | Nr,\|| | Nr, | Nr,\\| | Nr, | $\mathrm{Nr}_{\text {,\|\| }}$ | $\mathrm{Nr}_{, \perp}$ |
| $6.0 \times 40$ | 6 | 24 | 0.853 | 0.401 | 0.934 | 0.481 | 0.956 | 0.504 | 0.987 | 0.539 | 1.008 | 0.562 | 1.067 | 0.631 |
| $6.0 \times 60$ |  | 44 |  | 0.568 |  | 0.622 |  | 0.636 |  | 0.657 |  | 0.671 |  | 0.711 |
| $6.0 \times 80$ |  | 64 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 100$ |  | 84 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 120$ |  | 104 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 140$ |  | 124 |  |  |  |  |  |  |  |  |  |  |  |  |
| $6.0 \times 160$ |  | 144 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 60$ |  | 40 | 1.623 | 0.921 | 1.777 | 1.105 | 1.818 | 1.158 | 1.878 | 1.237 | 1.917 | 1.276 | 2.030 | 1.352 |
| $8.0 \times 80$ |  | 60 |  | 1.079 |  | 1.182 |  | 1.210 |  | 1.250 |  |  |  |  |
| $8.0 \times 100$ |  | 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 120$ |  | 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 160$ |  | 140 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 180$ |  | 160 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 200$ |  | 180 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 220$ |  | 200 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 240$ |  | 220 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 260$ |  | 240 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 280$ |  | 260 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 300$ |  | 280 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 340$ |  | 320 |  |  |  |  |  |  |  |  |  |  |  |  |
| $8.0 \times 380$ |  | 360 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 120$ |  | 98 | 2.356 | 1.567 | 2.578 | 1.715 | 2.638 | 1.756 | 2.726 | 1.814 | 2.782 | 1.852 | 2.945 | 1.961 |
| $10.0 \times 160$ |  | 138 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 200$ |  | 178 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 220$ |  | 198 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 240$ |  | 218 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 260$ |  | 238 |  |  |  |  |  |  |  |  |  |  |  |  |
| 10.0×280 |  | 258 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 300$ |  | 278 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 340$ |  | 318 |  |  |  |  |  |  |  |  |  |  |  |  |
| $10.0 \times 380$ |  | 358 |  |  |  |  |  |  |  |  |  |  |  |  |

## 2. Reference design values

Table 2.5: Continued

| Fastener <br> Designation <br> Diameter $\times$ <br> Length <br> (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member <br> Dowel <br> Bearing <br> Length ${ }^{5}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Steel-Wood Connections for Specific Gravities of $1,2,3,4$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 0.35 |  | 0.42 |  | 0.44 |  | 0.47 |  | 0.49 |  | 0.55 |
|  |  |  | Nr, | Nr, | Nr, | Nr, | Nr,\|| | Nr, | Nr,\||l | Nr, | Nr,\|| | Nr, | Nr, ${ }_{\text {,\|\| }}$ | Nr, |
| $13.0 \times 400$ | 6 | 377 | 4.176 | 2.777 | 4.570 | 3.041 | 4.677 | 3.112 | 4.832 | 3.216 | 4.932 | 3.283 | 5.222 | 3.477 |
| $13.0 \times 500$ |  | 477 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 600$ |  | 577 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 700$ |  | 677 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 800$ |  | 777 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 900$ |  | 877 |  |  |  |  |  |  |  |  |  |  |  |  |
| $13.0 \times 1000$ |  | 977 |  |  |  |  |  |  |  |  |  |  |  |  |

Notes:
(Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only,
${ }^{2}$ Tabulated reference lateral design values, $N_{r}$ apply to screws driven into the side grain of the main member, such that the screws are oriented perpendicular to the grain and loaded as follows:

- $\mathrm{N}_{\mathrm{r}, \mathrm{I}}$ main member is loaded parallel to the grain.
- $N_{r, \perp}$ main member is loaded perpendicular to the grain.
${ }^{3}$ Tabulated lateral design values are based on side member dowel bearing strength of 450 MPa for ASTM A36 steel.
${ }^{4}$ The value $f_{y}$ used in calculating tables 2.2-2.7 is the value $f_{y}{ }^{1}$ from Table 2.1
${ }^{5}$ Main member dowel bearing length, $\mathrm{t}_{2}$ is defined as fastener penetration into the main member minus the length of the tapered tip of the screw.

HTP \& WR

## 2. Reference design values

The reference lateral design values for SFS HTP and WR are provided in Tables 2.22.7. The factored withdrawal and factored head pull-through values are provided in Tables 2.8, 2.9 and 2.10 respectively. The appropriate modification values shall be used as described in Section 1.2 of this design guide.

Figure 2.5


Table 2.6: Reference lateral design values-wood-to-wood connection, $45^{\circ}$ angle to grain, full thread

| Fastener <br> Designation Diameter $\times$ Length (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main <br> Member <br> Embed- <br> ment <br> Length ${ }^{4}$, <br> $\mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Wood-Wood Connections, 45 degree angle to grain for Specific Gravities of $1,2,3$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.35 |  |  |  | 0.42 |  |  |  | 0.44 |
|  |  |  | $\mathrm{Nr}_{\\| \mid 1 / 45}$ | $\mathbf{N r}$,\||L $/ 45$ | $\mathrm{Nr}_{1,\\| \\| 45}$ | $\mathbf{N r}_{1}, 45$ | $\mathrm{Nr}_{\boldsymbol{\prime} \mid 1 / 45}$ | $\mathrm{Nr}_{\text {,\|\| }}$ / 45 | $\mathrm{Nr}_{\text {r }}$ | Nr, 1,45 | $\mathrm{Nr}_{\\| \mid 145}$ | $\mathbf{N r}$,\||L 4 , | $\mathrm{Nr}_{1, \\| \mid 1 / 45}$ | Nr, ${ }_{1,45}$ |
| $6.0 \times 80$ | 25 | 45 | 1.00 | 1.00 | 1.00 | 1.00 | 1.15 | 1.15 | 1.15 | 1.15 | 1.19 | 1.19 | 1.19 | 1.19 |
| $6.0 \times 100$ | 38 | 46 | 1.31 | 1.31 | 1.31 | 1.31 | 1.51 | 1.51 | 1.51 | 1.51 | 1.55 | 1.55 | 1.55 | 1.55 |
| $6.0 \times 120$ |  | 66 | 1.52 | 1.52 | 1.52 | 1.52 | 1.75 | 1.75 | 1.75 | 1.75 | 1.81 | 1.81 | 1.81 | 1.81 |
| $6.0 \times 140$ | 50 | 69 | 1.96 | 1.96 | 1.96 | 1.96 | 2.26 | 2.26 | 2.26 | 2.26 | 2.33 | 2.33 | 2.33 | 2.33 |
| $6.0 \times 160$ |  | 89 | 2.00 | 2.00 | 2.00 | 2.00 | 2.30 | 2.30 | 2.30 | 2.30 | 2.38 | 2.38 | 2.38 | 2.38 |
| $8.0 \times 100$ | 38 | 46 | 1.75 | 1.75 | 1.75 | 1.75 | 2.01 | 2.01 | 2.01 | 2.01 | 2.07 | 2.07 | 2.07 | 2.07 |
| $8.0 \times 120$ |  | 66 | 2.03 | 2.03 | 2.03 | 2.03 | 2.33 | 2.33 | 2.33 | 2.33 | 2.41 | 2.41 | 2.41 | 2.41 |
| $8.0 \times 160$ | 60 | 75 | 2.84 | 2.84 | 2.84 | 2.84 | 3.26 | 3.26 | 3.26 | 3.26 | 3.37 | 3.37 | 3.37 | 3.37 |
| $8.0 \times 180$ |  | 95 | 3.20 | 3.20 | 3.20 | 3.20 | 3.68 | 3.68 | 3.68 | 3.68 | 3.80 | 3.80 | 3.80 | 3.80 |
| $8.0 \times 200$ | 76 | 93 | 3.49 | 3.49 | 3.49 | 3.49 | 4.02 | 4.02 | 4.02 | 4.02 | 4.15 | 4.15 | 4.15 | 4.15 |
| $8.0 \times 220$ |  | 113 | 4.06 | 4.06 | 4.06 | 4.06 | 4.67 | 4.67 | 4.67 | 4.67 | 4.81 | 4.81 | 4.81 | 4.81 |
| $8.0 \times 240$ | 85 | 120 | 4.52 | 4.52 | 4.52 | 4.52 | 5.20 | 5.20 | 5.20 | 5.20 | 5.37 | 5.37 | 5.37 | 5.37 |
| $8.0 \times 260$ |  | 140 | 4.54 | 4.54 | 4.54 | 4.54 | 5.22 | 5.22 | 5.22 | 5.22 | 5.38 | 5.38 | 5.38 | 5.38 |
| $8.0 \times 280$ | 100 | 139 | 5.23 | 5.23 | 5.23 | 5.23 | 6.02 | 6.02 | 6.02 | 6.02 | 6.21 | 6.21 | 6.21 | 6.21 |
| $8.0 \times 300$ |  | 159 | 5.34 | 5.34 | 5.34 | 5.34 | 6.14 | 6.14 | 6.14 | 6.14 | 6.33 | 6.33 | 6.33 | 6.33 |
| $8.0 \times 340$ | 114 | 179 | 6.09 | 6.09 | 6.09 | 6.09 | 7.00 | 7.00 | 7.00 | 7.00 | 7.22 | 7.22 | 7.22 | 7.22 |
| $8.0 \times 380$ | 138 | 185 | 6.98 | 6.98 | 6.98 | 6.98 | 8.03 | 8.03 | 8.03 | 8.03 | 8.28 | 8.28 | 8.28 | 8.28 |
| $10.0 \times 120$ | 38 | 66 | 2.54 | 2.54 | 2.54 | 2.54 | 2.92 | 2.92 | 2.92 | 2.92 | 3.01 | 3.01 | 3.01 | 3.01 |
| $10.0 \times 160$ | 50 | 89 | 3.34 | 3.34 | 3.34 | 3.34 | 3.84 | 3.84 | 3.84 | 3.84 | 3.96 | 3.96 | 3.96 | 3.96 |
| $10.0 \times 200$ | 76 | 93 | 4.37 | 4.37 | 4.37 | 4.37 | 5.02 | 5.02 | 5.02 | 5.02 | 5.18 | 5.18 | 5.18 | 5.18 |
| $10.0 \times 220$ |  | 113 | 5.07 | 5.07 | 5.07 | 5.07 | 5.83 | 5.83 | 5.83 | 5.83 | 6.02 | 6.02 | 6.02 | 6.02 |
| $10.0 \times 240$ | 85 | 120 | 5.66 | 5.66 | 5.66 | 5.66 | 6.50 | 6.50 | 6.50 | 6.50 | 6.71 | 6.71 | 6.71 | 6.71 |
| $10.0 \times 260$ |  | 140 | 5.67 | 5.67 | 5.67 | 5.67 | 6.52 | 6.52 | 6.52 | 6.52 | 6.73 | 6.73 | 6.73 | 6.73 |
| $10.0 \times 280$ | 100 | 139 | 6.54 | 6.54 | 6.54 | 6.54 | 7.52 | 7.52 | 7.52 | 7.52 | 7.76 | 7.76 | 7.76 | 7.76 |
| $10.0 \times 300$ |  | 159 | 6.67 | 6.67 | 6.67 | 6.67 | 7.67 | 7.67 | 7.67 | 7.67 | 7.92 | 7.92 | 7.92 | 7.92 |
| $10.0 \times 340$ | 120 | 170 | 8.01 | 8.01 | 8.01 | 8.01 | 9.21 | 9.21 | 9.21 | 9.21 | 9.50 | 9.50 | 9.50 | 9.50 |
| $10.0 \times 380$ | 138 | 185 | 8.73 | 8.73 | 8.73 | 8.73 | 10.03 | 10.03 | 10.03 | 10.03 | 10.35 | 10.35 | 10.35 | 10.35 |
| $13.0 \times 400$ |  | 205 | 11.97 | 11.97 | 11.97 | 11.97 | 13.77 | 13.77 | 13.77 | 13.77 | 14.21 | 14.21 | 14.21 | 14.21 |
| $13.0 \times 500$ | 175 | 253 | 15.18 | 15.18 | 15.18 | 15.18 | 17.46 | 17.46 | 17.46 | 17.46 | 18.01 | 18.01 | 18.01 | 18.01 |
| $13.0 \times 600$ | 215 | 296 | 18.16 | 18.16 | 18.16 | 18.16 | 20.88 | 20.88 | 20.88 | 20.88 | 21.55 | 21.55 | 21.55 | 21.55 |
| $13.0 \times 700$ | 252 | 344 | 21.09 | 21.09 | 21.09 | 21.09 | 24.25 | 24.25 | 24.25 | 24.25 | 25.02 | 25.02 | 25.02 | 25.02 |
| $13.0 \times 800$ | 275 | 411 | 23.86 | 23.86 | 23.86 | 23.86 | 27.43 | 27.43 | 27.43 | 27.43 | 28.31 | 28.31 | 28.31 | 28.31 |
| $13.0 \times 900$ | 330 | 433 | 26.59 | 26.59 | 26.59 | 26.59 | 30.57 | 30.57 | 30.57 | 30.57 | 31.12 | 31.12 | 31.12 | 31.12 |
| $13.0 \times 1000$ | 350 | 505 | 30.37 | 30.37 | 30.37 | 30.37 | 31.12 | 31.12 | 31.12 | 31.12 |  |  |  |  |

## HTP \& WR

## 2. Reference design values

Table 2.6: Continued

| Fastener Designation Diameter $\times$ Length (mm) | Side <br> Member Thickness, $t_{1}$ (mm) | Main <br> Member Embedment Length ${ }^{4}$, $\mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Wood-Wood Connections, 45 degree angle to grain for Specific Gravities of ${ }^{1,2,3}$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | 0.47 |  |  |  | 0.49 |  |  |  | 0.55 |
|  |  |  | $\mathbf{N r}$,\|lı45 | $\mathrm{Nr}_{\\|\| \| 1,45}$ | $\mathrm{Nr}_{1 \perp\| \|, 45}$ | Nr, ${ }^{\prime}$, 45 | $\mathbf{N r}{ }_{\text {, }}$, 45 | $\mathrm{Nr}_{\text {,\|\| }}{ }_{1,45}$ | $\mathrm{Nr}_{\lrcorner \perp\\| \\| 45}$ | Nr,1,45 | $\mathbf{N r}$,\||,45 | Nr, \|| ${ }_{1}$,45 | $\mathrm{Nr}, \perp\\| \\| 45$ | Nr, 1,45 |
| $6.0 \times 80$ | 25 | 45 | 1.25 | 1.25 | 1.25 | 1.25 | 1.30 | 1.30 | 1.30 | 1.30 | 1.41 | 1.41 | 1.41 | 1.41 |
| $6.0 \times 100$ | 38 | 46 | 1.63 | 1.63 | 1.63 | 1.63 | 1.70 | 1.70 | 1.70 | 1.70 | 1.85 | 1.85 | 1.85 | 1.85 |
| $6.0 \times 120$ |  | 66 | 1.90 | 1.90 | 1.90 | 1.90 | 1.97 | 1.97 | 1.97 | 1.97 | 2.15 | 2.15 | 2.15 | 2.15 |
| $6.0 \times 140$ | 50 | 69 | 2.45 | 2.45 | 2.45 | 2.45 | 2.54 | 2.54 | 2.54 | 2.54 | 2.77 | 2.77 | 2.77 | 2.77 |
| $6.0 \times 160$ |  | 89 | 2.50 | 2.50 | 2.50 | 2.50 | 2.59 | 2.59 | 2.59 | 2.59 | 2.83 | 2.83 | 2.83 | 2.83 |
| $8.0 \times 100$ | 38 | 46 | 2.18 | 2.18 | 2.18 | 2.18 | 2.26 | 2.26 | 2.26 | 2.26 | 2.47 | 2.47 | 2.47 | 2.47 |
| $8.0 \times 120$ |  | 66 | 2.53 | 2.53 | 2.53 | 2.53 | 2.63 | 2.63 | 2.63 | 2.63 | 2.87 | 2.87 | 2.87 | 2.87 |
| $8.0 \times 160$ | 60 | 75 | 3.54 | 3.54 | 3.54 | 3.54 | 3.67 | 3.67 | 3.67 | 3.67 | 4.01 | 4.01 | 4.01 | 4.01 |
| $8.0 \times 180$ |  | 95 | 3.99 | 3.99 | 3.99 | 3.99 | 4.15 | 4.15 | 4.15 | 4.15 | 4.52 | 4.52 | 4.52 | 4.52 |
| $8.0 \times 200$ | 76 | 93 | 4.36 | 4.36 | 4.36 | 4.36 | 4.52 | 4.52 | 4.52 | 4.52 | 4.94 | 4.94 | 4.94 | 4.94 |
| $8.0 \times 220$ |  | 113 | 5.06 | 5.06 | 5.06 | 5.06 | 5.25 | 5.25 | 5.25 | 5.25 | 5.73 | 5.73 | 5.73 | 5.73 |
| $8.0 \times 240$ | 85 | 120 | 5.64 | 5.64 | 5.64 | 5.64 | 5.86 | 5.86 | 5.86 | 5.86 | 6.39 | 6.39 | 6.39 | 6.39 |
| $8.0 \times 260$ |  | 140 | 5.66 | 5.66 | 5.66 | 5.66 | 5.88 | 5.88 | 5.88 | 5.88 | 6.41 | 6.41 | 6.41 | 6.41 |
| $8.0 \times 280$ | 100 | 139 | 6.53 | 6.53 | 6.53 | 6.53 | 6.78 | 6.78 | 6.78 | 6.78 | 7.39 | 7.39 | 7.39 | 7.39 |
| $8.0 \times 300$ |  | 159 | 6.66 | 6.66 | 6.66 | 6.66 | 6.91 | 6.91 | 6.91 | 6.91 | 7.54 | 7.54 | 7.54 | 7.54 |
| $8.0 \times 340$ | 114 | 179 | 7.59 | 7.59 | 7.59 | 7.59 | 7.88 | 7.88 | 7.88 | 7.88 | 8.60 | 8.60 | 8.60 | 8.60 |
| $8.0 \times 380$ | 138 | 185 | 8.70 | 8.70 | 8.70 | 8.70 | 9.04 | 9.04 | 9.04 | 9.04 | 9.86 | 9.86 | 9.86 | 9.86 |
| $10.0 \times 120$ | 38 | 66 | 3.16 | 3.16 | 3.16 | 3.16 | 3.28 | 3.28 | 3.28 | 3.28 | 3.58 | 3.58 | 3.58 | 3.58 |
| $10.0 \times 160$ | 50 | 89 | 4.16 | 4.16 | 4.16 | 4.16 | 4.32 | 4.32 | 4.32 | 4.32 | 4.71 | 4.71 | 4.71 | 4.71 |
| $10.0 \times 200$ | 76 | 93 | 5.45 | 5.45 | 5.45 | 5.45 | 5.65 | 5.65 | 5.65 | 5.65 | 6.17 | 6.17 | 6.17 | 6.17 |
| $10.0 \times 220$ |  | 113 | 6.32 | 6.32 | 6.32 | 6.32 | 6.57 | 6.57 | 6.57 | 6.57 | 7.16 | 7.16 | 7.16 | 7.16 |
| $10.0 \times 240$ | 85 | 120 | 7.05 | 7.05 | 7.05 | 7.05 | 7.32 | 7.32 | 7.32 | 7.32 | 7.99 | 7.99 | 7.99 | 7.99 |
| $10.0 \times 260$ |  | 140 | 7.07 | 7.07 | 7.07 | 7.07 | 7.34 | 7.34 | 7.34 | 7.34 | 8.01 | 8.01 | 8.01 | 8.01 |
| $10.0 \times 280$ | 100 | 139 | 8.16 | 8.16 | 8.16 | 8.16 | 8.47 | 8.47 | 8.47 | 8.47 | 9.24 | 9.24 | 9.24 | 9.24 |
| $10.0 \times 300$ |  | 159 | 8.32 | 8.32 | 8.32 | 8.32 | 8.64 | 8.64 | 8.64 | 8.64 | 9.43 | 9.43 | 9.43 | 9.43 |
| $10.0 \times 340$ | 120 | 170 | 9.99 | 9.99 | 9.99 | 9.99 | 10.37 | 10.37 | 10.37 | 10.37 | 11.31 | 11.31 | 11.31 | 11.31 |
| $10.0 \times 380$ | 138 | 185 | 10.88 | 10.88 | 10.88 | 10.88 | 11.30 | 11.30 | 11.30 | 11.30 | 12.32 | 12.32 | 12.32 | 12.32 |
| $13.0 \times 400$ |  | 205 | 14.93 | 14.93 | 14.93 | 14.93 | 15.50 | 15.50 | 15.50 | 15.50 | 16.91 | 16.91 | 16.91 | 16.91 |
| $13.0 \times 500$ | 175 | 253 | 18.93 | 18.93 | 18.93 | 18.93 | 19.66 | 19.66 | 19.66 | 19.66 | 21.45 | 21.45 | 21.45 | 21.45 |
| $13.0 \times 600$ | 215 | 296 | 22.65 | 22.65 | 22.65 | 22.65 | 23.51 | 23.51 | 23.51 | 23.51 | 25.65 | 25.65 | 25.65 | 25.65 |
| $13.0 \times 700$ | 252 | 344 | 26.29 | 26.29 | 26.29 | 26.29 | 27.30 | 27.30 | 27.30 | 27.30 | 29.79 | 29.79 | 29.79 | 29.79 |
| $13.0 \times 800$ | 275 | 411 | 29.75 | 29.75 | 29.75 | 29.75 | 30.89 | 30.89 | 30.89 | 30.89 | 31.12 | 31.12 | 31.12 | 31.12 |
| $13.0 \times 900$ | 330 | 433 | 31.12 | 31.12 | 31.12 | 31.12 | 31.12 | 31.12 | 31.12 | 31.12 |  |  |  |  |
| $13.0 \times 1000$ | 350 | 505 |  |  |  |  |  |  |  |  |  |  |  |  |

Notes:
${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
${ }^{2}$ Tabulated reference lateral design values, $\mathrm{N}_{\mathrm{r}}$ apply to screws driven into the side grain of the main member, such that the screws are oriented 45 degrees to the grain. - $N_{r, \|, 45}$ both side and main member are loaded parallel to the grain.

- $\mathrm{N}_{\mathrm{r}, \| / 1,45}$ side member loaded perpendicular to the grain and main member loaded parallel to the grain.
- $\mathrm{N}_{\mathrm{r}, \perp / \|, 45}$ side member loaded parallel to the grain and main member loaded perpendicular to the grain.
$-N_{r, 1,45}$ both side and main member are loaded perpendicular to the grain.
${ }^{3}$ The value $\mathrm{f}_{y}$ used in calculating tables $2.2-2.7$ is the value $\mathrm{f}_{\mathrm{y}}{ }^{1}$ from Table 2.1
 of screw).


## 2. Reference design values

The reference lateral design values for SFS HTP and WR are provided in Tables 2.22.7. The factored withdrawal and factored head pull-through values are provided in Tables $2.8,2.9$ and 2.10 respectively. The appropriate modification values shall be used as described in Section 1.2 of this design guide

Figure 2.6


Table 2.7: Reference lateral design values-steel-to-wood connection, $45^{\circ}$ angle to grain, full thread


## 2. Reference design values

Table 2.7: Continued

| Fastener <br> Designation <br> Diameter $\times$ <br> Length <br> (mm) | Side <br> Member Thickness, $\mathrm{t}_{1}$ (mm) | Main Member Embedment Depth ${ }^{4}, \mathrm{t}_{2}$ (mm) | Factored Lateral Resistance (kN) for Full Thread Screws in Steel-Wood Connections for Specific Gravities of $1,2,3$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0.35 | 0.42 | 0.44 | 0.47 | 0.49 | 0.55 |
|  |  |  | $\mathrm{Nr}_{\\| \mid 1 / 45}$ | $\mathbf{N r}_{\\| \mid 1 / 45}$ | $\mathrm{Nr}_{\\| \mid 1 / 45}$ | $\mathrm{Nr}_{\boldsymbol{\\|} / 145}$ | $\mathrm{Nr}_{\boldsymbol{\\|} \\| \text { \|/45 }}$ | $\mathbf{N r}{ }_{\\| \mid 1,45}$ |
| $13.0 \times 800$ | 6 | 791 | 31.12 | 31.12 | 31.12 | 31.12 | 31.12 | 31.12 |
| $13.0 \times 900$ |  | 891 |  |  |  |  |  |  |
| $13.0 \times 1000$ |  | 991 |  |  |  |  |  |  |

Notes:
${ }^{1}$ Values must be multiplied by all applicable adjustment factors, in accordance with CSA 086:19. For use in dry conditions only.
${ }^{2}$ Tabulated lateral design values are based on side member dowel bearing strength of 450 MPa for ASTM A36 steel.
${ }^{3}$ The value $\mathrm{f}_{\mathrm{y}}$ used in calculating tables $2.2-2.7$ is the value $\mathrm{f}_{\mathrm{y}}{ }^{1}$ from Table 2.1
${ }^{4}$ Main member embedment length, $\mathrm{t}_{2}$ is defined as fastener penetration into the main member including the length of the tapered tip of the screw (measured along actual length of screw).

## 2. Reference design values

Figure 2.7.1


Figure 2.7.2



|  | Factored withdrawal resistance, $\mathrm{P}_{\mathrm{rw}}$ (kN/20 mm embedment) for $\mathbf{G}$ |  |  |  |  |  |  |  |  | Factored tensile resistance, $\mathrm{T}_{\mathrm{r}}$ <br> (kN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Screw | d (mm) | 0.35 | 0.42 | 0.44 | 0.46 | 0.47 | 0.49 | 0.50 | 0.55 |  |
| HTP 6 mm | 6.0 | 0.80 | 0.92 | 0.95 | 0.99 | 1.00 | 1.04 | 1.06 | 1.13 | 9.04 |
| HTP 8 mm | 8.0 | 1.07 | 1.23 | 1.27 | 1.32 | 1.33 | 1.38 | 1.41 | 1.51 | 16.00 |
| HTP 10 mm | 10.0 | 1.34 | 1.54 | 1.59 | 1.65 | 1.67 | 1.73 | 1.76 | 1.89 | 24.00 |
| WR | 13.0 | 1.74 | 2.00 | 2.06 | 2.14 | 2.17 | 2.25 | 2.29 | 2.45 | 44.00 |

${ }^{1}$ Factored withdrawal per 20 mm embedment and using $\mathrm{Kd}=1$, Фequiv (standard adjustment factor) $=0.77$
${ }^{2}$ Calculated withdrawal value must not exceed factored tensile resistance, $T_{r}$ of the screw
${ }^{3}$ Factored withdrawal, $\mathrm{P}_{\mathrm{rw}}$, includes the length of the tapered tip of the self-tapping screws when considering the embedment depth.
${ }^{4} n_{\text {ef }}$, the effective number of screws in the connection, may be taken to be 1.0 ; however, a more conservative value can be applied as follows:
$n_{\text {ef }}=\max \{n 0.9 ; 0.9 \cdot n\} \quad$ (Eq. 2-1)

Table 2.9: Alternate reference table for factored withdrawal resistance, $\mathbf{P}_{\mathrm{rw}}(\mathbf{k N} / \mathbf{m m})$ for $\mathbf{G}^{1,2,3,4}$

|  | Factored withdrawal resistance, $\mathrm{P}_{\text {rw }}$ (kN/mm embedment) for $\mathbf{G}$ |  |  |  |  |  |  |  |  | Factored tensile resistance, $\mathrm{T}_{\mathrm{r}}$ (kN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Screw | d (mm) | 0.35 | 0.42 | 0.44 | 0.46 | 0.47 | 0.49 | 0.50 | 0.55 |  |
| HTP 6 mm | 6.0 | 0.040 | 0.046 | 0.048 | 0.050 | 0.050 | 0.052 | 0.053 | 0.057 | 9.04 |
| HTP 8 mm | 8.0 | 1.054 | 0.062 | 0.064 | 0.066 | 0.067 | 0.069 | 0.071 | 0.076 | 16.00 |
| HTP 10 mm | 10.0 | 0.067 | 0.077 | 0.080 | 0.083 | 0.084 | 0.087 | 0.088 | 0.095 | 24.00 |
| WR | 13.0 | 0.087 | 0.100 | 0.103 | 0.107 | 0.109 | 0.113 | 0.115 | 0.123 | 44.00 |

[^1]
## 2. Reference design values

Figure 2.8


Table 2.10: Factored head pull through resistance, $\mathrm{P}_{\mathrm{rh}}(\mathbf{k N})$ and factored tensile resistance, $\mathrm{T}_{\mathrm{r}}{ }^{1}$

|  | Factored head pull-through resistance, $\mathrm{P}_{\mathrm{rh}}(\mathbf{k N})$ for $\mathbf{G}$ |  |  |  |  |  |  |  |  | Factored tensile resistance, $\mathrm{T}_{\mathrm{r}}$ (kN) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Screw | $\mathrm{d}_{\mathrm{h}}{ }^{2}$ (mm) | 0.35 | 0.42 | 0.44 | 0.46 | 0.47 | 0.49 | 0.50 | 0.55 |  |
| HTP 6 mm countersunk | 11.7 | 1.09 | 1.25 | 1.29 | 1.34 | 1.35 | 1.40 | 1.43 | 1.53 | 9.04 |
| HTP 8 mm countersunk | 14.8 | 1.74 | 2.00 | 2.06 | 2.14 | 2.16 | 2.25 | 2.29 | 2.45 | 16.00 |
| HTP 10 mm countersunk | 18.5 | 2.71 | 3.12 | 3.22 | 3.35 | 3.38 | 3.51 | 3.58 | 3.83 | 24.00 |
| HTP 8mm hex | 13.0 | 1.34 | 1.54 | 1.59 | 1.65 | 1.67 | 1.73 | 1.77 | 1.89 | 16.00 |
| HTP 10 mm hex | 15.0 | 1.78 | 2.05 | 2.12 | 2.20 | 2.22 | 2.31 | 2.35 | 2.52 | 24.00 |
| HTP 6 mm flange | 14.0 | 1.55 | 1.79 | 1.84 | 1.92 | 1.94 | 2.01 | 2.05 | 2.19 | 9.04 |
| HTP 8 mm flange | 18.0 | 2.57 | 2.95 | 3.05 | 3.17 | 3.20 | 3.32 | 3.39 | 3.63 | 16.00 |
| HTP 10 mm flange | 22.5 | 4.01 | 4.61 | 4.76 | 4.96 | 5.00 | 5.20 | 5.29 | 5.67 | 24.00 |
| WR 13 mm countersunk | 22.0 | 3.84 | 4.41 | 4.55 | 4.74 | 4.78 | 4.97 | 5.06 | 5.42 | 44.00 |

[^2]
## 3. Connection geometry requirements

3.1: Connection geometry requirements without pre-drill

### 3.1.1: Lateral loading-in-line rows

Figure 3.1: Tension loading-parallel to grain

$$
0.35<\mathrm{G}<0.50
$$

$$
0.50<\mathrm{G}<0.55
$$




Figure 3.2: Compression loading-parallel to grain


## 3. Connection geometry requirements

Figure 3.3: Lateral loading-perpendicular to grain
Note: Values in parenthesis( ) apply to 10 mm and 13 mm screws only


### 3.1.2: Lateral loading-staggered rows

Note: Values apply to 6 mm and 8 mm screws
Figure 3.4: Tension loading-parallel to grain


Figure 3.5: Compression loading-parallel to grain


## 3. Connection geometry requirements

Figure 3.6: Lateral loading-perpendicular to grain


### 3.1.3: Axial loading

Figure 3.7: Axial loading (for all values of G)
Note: Values in parenthesis( ) apply to 10 mm and 13 mm screws only


### 3.1.4: Reference spacing

Table 3.1: Spacing table

|  | Screw diameter (mm) |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
|  | $\mathbf{6}$ | $\mathbf{8}$ | $\mathbf{1 0}$ | $\mathbf{1 3}$ |
| 2.5 D | 3 | 4 | 5 | 6.5 |
| 3D | 18 | 24 | 30 | 39 |
| 4 D | 24 | 32 | 40 | 52 |
| 5D | 30 | 40 | 50 | 65 |
| 7D | 42 | 56 | 70 | 91 |
| 10D | 60 | 80 | 100 | 130 |
| 12D | 72 | 96 | 120 | 156 |
| 15D | 190 | 120 | 150 | 195 |
| 20D | 120 | 160 | 200 | 260 |

## 3. Connection geometry requirements

## 3.2: Connection geometry requirements with pre-drill (for all values of G )

### 3.2.1: Lateral loading-in-line rows

Values in parenthesis ( ) apply to 10 mm and 13 mm screws only

Figure 3.8: Tension loading-parallel to grain


Figure 3.9: Compression loading-parallel to grain


Figure 3.10: Lateral loading-perpendicular to grain
Values in parenthesis ( ) apply to 10 mm and 13 mm screws only


## 3. Connection geometry requirements

3.2.2: Lateral loading-staggered rows

Values only apply for 6 mm and 8 mm screws
Figure 3.11: Tension loading-parallel to grain


Figure 3.12: Compression loading-parallel to grain


Figure 3.13: Lateral loading-perpendicular to grain


## 3. Connection geometry requirements

### 3.2.3: Axial loading

Figure 3.14: Axial loading
Values in parenthesis () apply to 10 mm and 13 mm screws only

3.2.4: Reference spacing

Table 3.2: Spacing table

|  | Screw diameter (mm) |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
|  | $\mathbf{6}$ | $\mathbf{8}$ | $\mathbf{1 0}$ | $\mathbf{1 3}$ |
| 2.5 D | 3 | 4 | 5 | 6.5 |
| 3D | 18 | 24 | 30 | 39 |
| 4D | 24 | 32 | 40 | 52 |
| 5D | 30 | 40 | 50 | 65 |
| 7D | 42 | 56 | 70 | 91 |
| 10D | 60 | 80 | 100 | 130 |
| 12D | 72 | 96 | 120 | 156 |
| 15D | 190 | 120 | 150 | 195 |
| 20D | 120 | 160 | 200 | 260 |

## 4. Withdrawal at an angle to grain

Apply the following equation to reduce the reference withdrawal design value when screws are inserted at an angle to grain.

## Reference withdrawal design value adjustments

Reference withdrawal design values ( $P_{r w, \alpha}$ ) in $\mathrm{kN} / \mathrm{mm}$ of thread penetration for screws installed at an angle $\alpha$ (in degrees) to the grain of the wood member must be determined as follows:
$P_{r w, \alpha}=P_{r w} \cdot k_{\alpha}$

Where:
$P_{r w}=$ The reference withdrawal design value for $\alpha=90^{\circ}$ determined in accordance with Table 2.8.
$\mathrm{k}_{\alpha}=$ Value from table 4.1

## Table 4.1

Values of $\mathrm{k}_{\alpha}$ for standard angles:

| $\alpha$ | $\mathbf{k}_{\alpha}$ | $\alpha$ | $\mathbf{k}_{\alpha}$ |
| :---: | :---: | :---: | :---: |
| 90 | 1.00 | 40 | 0.89 |
| 85 |  | 35 | 0.84 |
| 80 |  | 30 | 0.77 |
| 75 |  | 25 | 0.69 |
| 70 |  | 20 | 0.61 |
| 65 |  | 15 | 0.53 |
| 60 |  | 14* | 0.52 |
| 55 |  | 10* | 0.46 |
| 50 |  | 5* | 0.38 |
| 45 |  | 0* | 0.30 |

* At least four (4) screws required for structural connections with $\alpha<15^{\circ}$

Figure 4.1


Figure 4.2


## HTP \& WR

## 5. Combined lateral and withdrawal loading

For cases of combined lateral and withdrawal loading, the following expression should be satisfied:

$$
\left(\mathrm{P}_{\mathrm{ax}} / P_{\mathrm{rw}}\right)^{2}+\left(\mathrm{P}_{\mathrm{v}} / N_{\mathrm{r}}\right)^{2} \leq 1 \quad(\text { Eq. } 5-1)
$$

Where:
$P_{f, a x}=$ factored axial force on fastener
$P_{r w}=$ factored withdrawal resistance of fastener (See Table 2.8)
$P_{f, v}=$ factored lateral force on fastener
$N_{r}=$ factored lateral resistance of fastener (See Tables 2.2-2.7)

## Figure 5.1



## HTP \& WR

## 6. Compressive capacity for fully threaded screws

For screws in compression the following must be satisfied:
$C_{r}=\min \left\{P_{r w}, C_{r b}\right\}($ Eq. 6-1)

Where:
$P_{\text {rw }}=$ Factored withdrawal resistance (kN) from Table 2.8
$\mathrm{C}_{\text {rb }}=$ Factored compression (buckling) resistance (kN) from Table 6.1

## Table 6.1

Factored Compression (Buckling) Resistance ( $\mathrm{C}_{\mathrm{rb}}$ ) in kN

| $\mathbf{d}$ |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\mathbf{d}$ | $\mathbf{0 . 3 5}$ | $\mathbf{0 . 4 2}$ | $\mathbf{0 . 4 4}$ | $\mathbf{0 . 4 6}$ | $\mathbf{0 . 4 7}$ | $\mathbf{0 . 4 9}$ | $\mathbf{0 . 5 5}$ |
| $\mathbf{( m m )}$ | $\mathbf{0 . 0}$ | 6.8 |  |  |  |  |  |
| 6 | 6.0 | 6.3 | 6.4 | 6.5 | 6.5 | 6.6 | 6.8 |
| 8 | 11.1 | 11.6 | 11.7 | 11.8 | 11.9 | 12.0 | 12.3 |
| 10 | 15.4 | 16.0 | 16.2 | 16.3 | 16.4 | 16.6 | 16.9 |
| 13 | 30.1 | 31.4 | 31.6 | 32.0 | 32.1 | 32.4 | 33.2 |

Note: Compression (buckling) resistance for self-tapping screws in timber assemblies is expressed as a single value, independent of the length of the screw.

Figure 6.1


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[^0]:    ${ }^{1}$ Hexagon head has 13 mm hex drive with T40 internal drive and 15 mm hex drive with T40 internal drive for diameters $5 / 16^{\prime \prime}(8 \mathrm{~mm})$ and $3 / 8^{\prime \prime}(10 \mathrm{~mm})$, respectively ${ }^{2}$ Only applies to partial thread (PT) screws.

[^1]:    ${ }^{1}$ Factored withdrawal per 20 mm embedment and using $\mathrm{Kd}=1$, Фequiv (standard adjustment factor) $=0.77$
    ${ }^{2}$ Calculated withdrawal value must not exceed factored tensile resistance, $T_{r}$ of the screw
    ${ }^{3}$ Factored withdrawal, Prw, includes the length of the tapered tip of the self-tapping screws when considering the embedment depth.
    ${ }^{4} n_{\text {eff }}$, the effective number of screws in the connection, may be taken to be 1.0; however, a more conservative value can be applied as follows:
    $n_{\text {ef }}=\max \{n 0.9 ; 0.9 \cdot n\} \quad$ (Eq. 2-1)

[^2]:    ${ }^{1}$ Factored pull-through resistance based on minimum member thickness of 20 mm and using $\mathrm{Kd}=1$, ©equiv (standard adjustment factor) $=0.77$
    ${ }^{2} \mathrm{~d}_{\mathrm{h}}$ refers to screw head diameter.
    ${ }^{3}$ Calculated withdrawal value must not exceed factored tensile resistance, $T_{r}$ of the screw

